



**TECHNISCHE
UNIVERSITÄT
DRESDEN**

Fakultät Maschinenwesen

Institut für Energietechnik

Lehrstuhl für Kälte- und Kryotechnik



Helium Refrigeration for sc Accelerators

SRF 2009 Tutorial Rossendorf

**Ch. Haberstroh
Sept. 19th, 2009**



Outline

- **introduction**
- **fluid properties of He**
- **liquefaction history**
- **theory of refrigeration cycles**
- **plant components**
- **2 K systems**
- **efficiencies**
- **He resources**



Professorship for Refrigeration and Cryogenics at TU Dresden:

1993 – 2008: Prof. Dr. H. Quack (before: Sulzer Cryogenics, Swiss)

actually (provisional): Dr. rer. nat. et Ing. habil. Ch. Haberstroh

ca. 12 permanent members, mostly Ph.D. students

- Teaching:**
- Refrigeration
 - Compressor Technology
 - **Kryo Technology**

- Research:**
- ...
 - ...
 - **Helium, Hydrogen Technology; Conceptual design for large Helium Plants**
He / H₂ Liquefiers, Dewar optimization, Neon cooling, ...
responsible for the central Helium Plant TU Dresden
co-operation with DESY, CERN, Rossendorf, GSI, BESSY, SLAC, FNAL, ...

sc Accelerator Cooling Task

Demand: Refrigeration at $\sim 5 \text{ K} \dots 1.7 \text{ K}$
 + thermal shield @ $\sim 20 \text{ K} \dots 100 \text{ K}$
 heat load: $10 \text{ W} \dots \text{kW}$ range

plus:
 high efficiency, high reliability,
 low noise level,
 low invest costs,
 8000 h continuous operation, ...

way to go: helium refrigeration cycles

cryogenic fluids:

	normal boiling point	price (m ³ gas)	
LN ₂	77 K	0.15 €	⇐ pre-cooling only
LNe	27 K	150 €	
LH ₂	20 K	0.50 €	
L ⁴ He	4.2 K	10 € (rising)	⇐ standard working fluid
L ³ He	3.2 K	250 000 €	⇐ extremely expensive, for closed mK coolers only



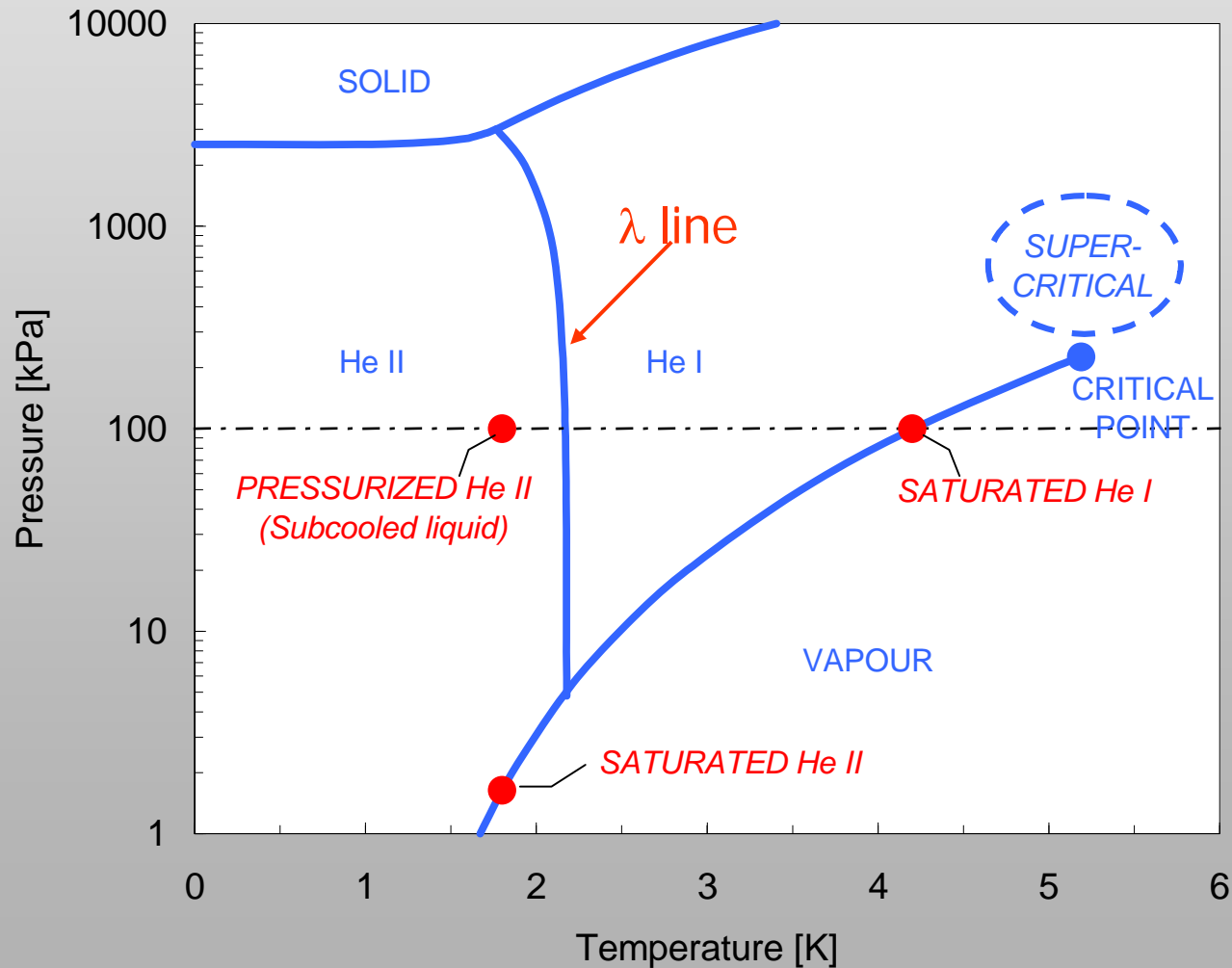
Helium (^4He)

- ideal cooling fluid:**
- + chemically inert, nontoxic, odorless
 - + high heat conductivity
 - + radiological inert
 - + high ionization energy
 - + low solubility
 - + extrem low boiling point

as well a few drawbacks:

- price, shortages ⇐ helium recovery, closed refrigeration cycles
- low evaporation enthalpy ⇐ nearly perfect thermal isolation
- low molecular mass ⇐ hard for turbo pumps or expanders
- high diffusion rates ⇐ special materials, sealings

^4He Phase Diagramm

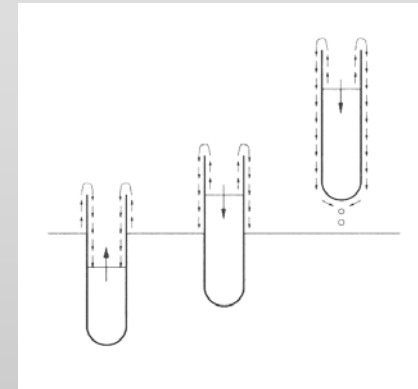


Ph. Lebrun, 2009

Superfluid Helium

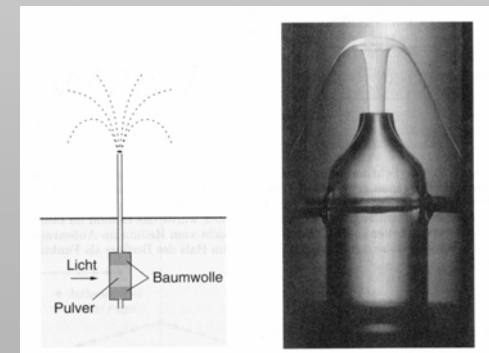
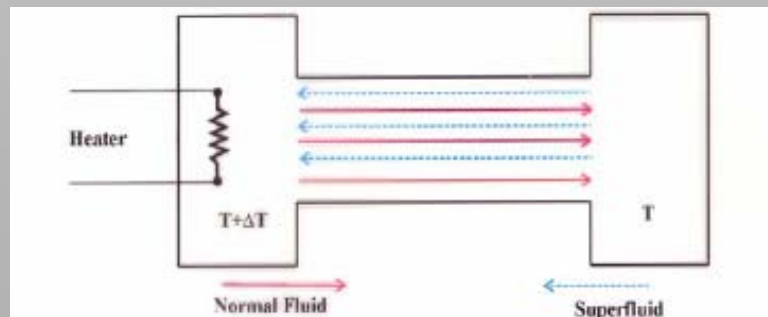
LHe I:
„normal“ liquid
nucleate boiling
at saturation line

LHe II:
superfluid helium
strange behavior
 $\lambda_{\text{He II}} \approx 10^6 \cdot \lambda_{\text{He I}}$
apparently no viscosity
quietly boiling from the
surface only



film creeping

explained by „two-fluid“ model
below λ line: normal + superfluid phase
two interpenetrating fluids, no friction



thermocoloric
(fountain) effect

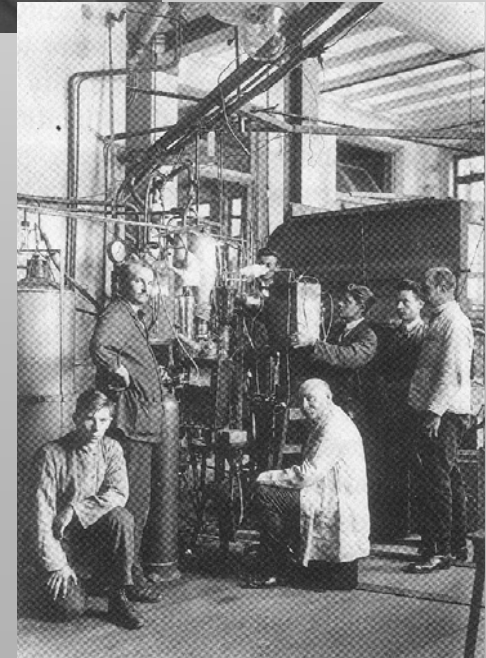
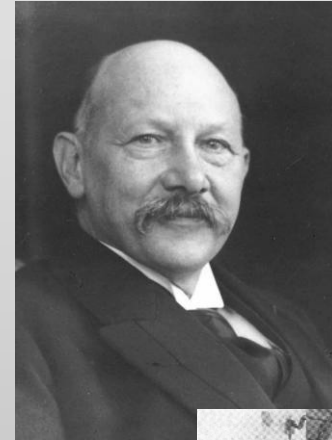


Helium Liquefaction

**first time by Heike Kamerlingh Onnes,
Leiden University,
July 10th, 1908**

Helium from monazite sand

**next 15 years: exclusive LHe laboratory
discovery of supraconductivity,
superfluidity, ...**



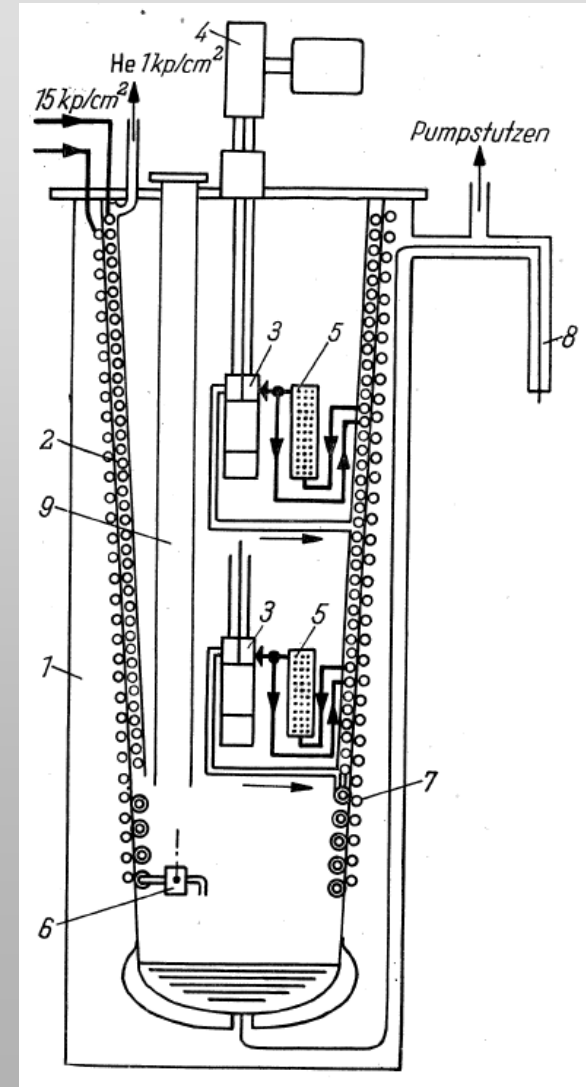
Commercial Liquefier Breakthrough



**Prof. Samuel Collins,
MIT/Boston
1946**

use of piston expanders

capacity: 10 l/h



Collins Liquefier

1946 – 1964 about 250 units sold
“revolution” in cryogenic research

Manufacturer:

A.D. Little Company ⇒ 500 Inc. ⇒ CTi

⇒ HPS ⇒ KPS ⇒ PSI ⇒ CPS/Linde

nevertheless basically unchanged

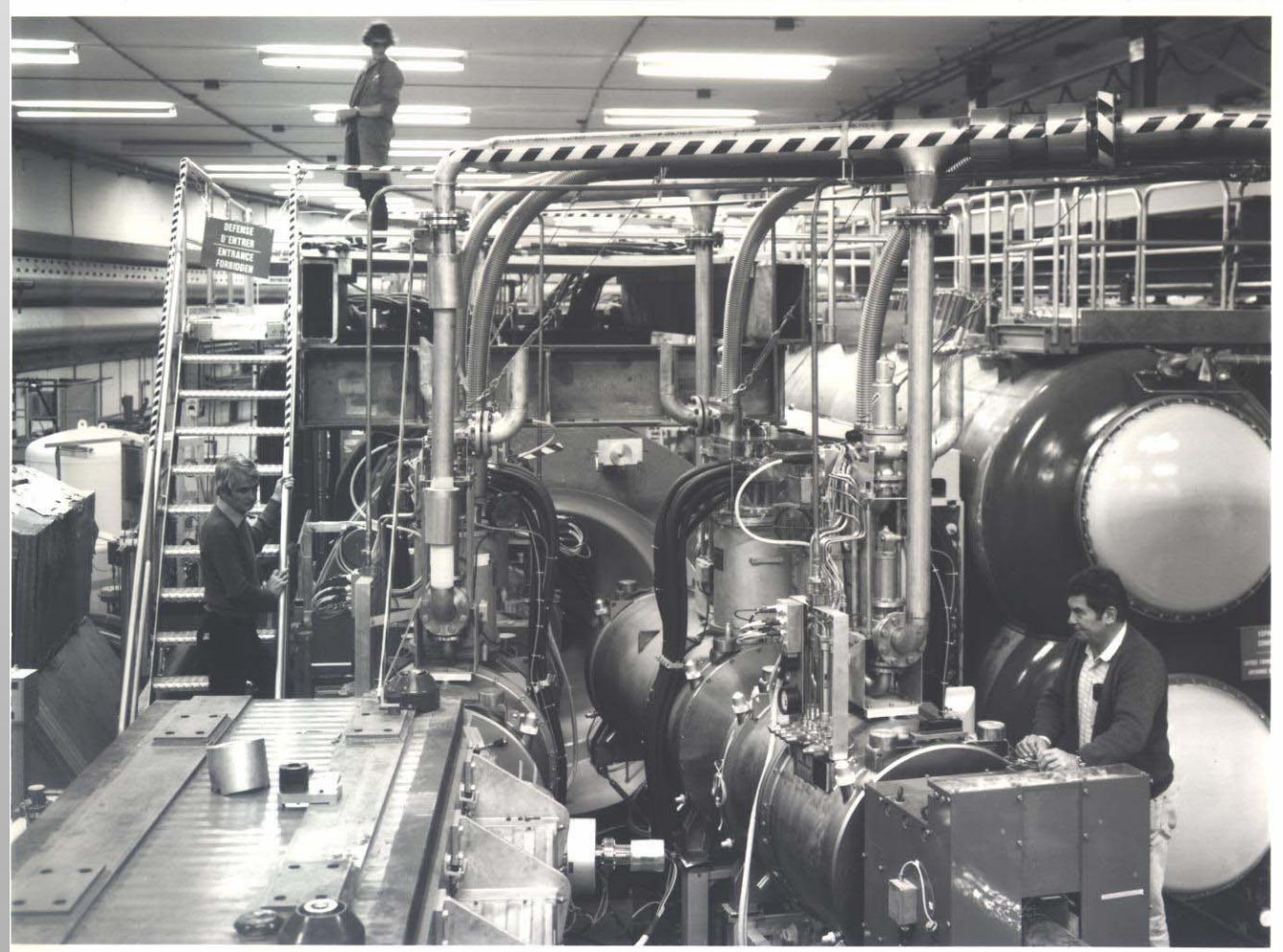
capacity: 12 ... 70 l/h



First sc Accelerator Magnets

implemented
in the 70th

(CERN, Fermilab)



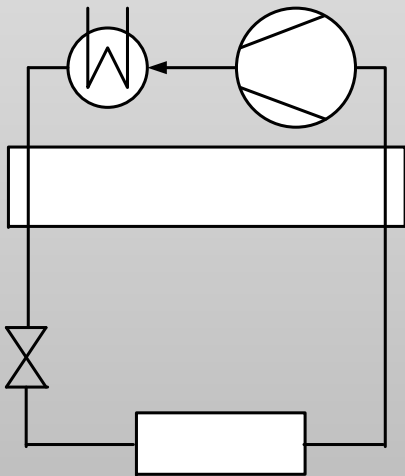
Helium Plants Today



LHC Cold Box
18 kW @ 4.5 K

33 kW @ 50 K ... 75 K
+
23 kW @ 4.6 K ... 20 K
+
41 g/s liquefaction

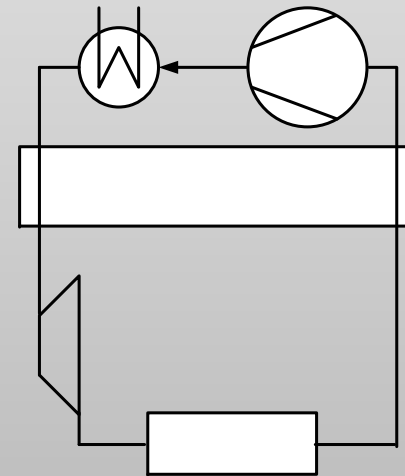
Theory: how to get a gas cold?



a) Joule-Thomson-Effect
simple throttle valve, isenthalpic
expansion (without work extraction)

$$\Delta H = 0$$

⇔ small effect (real gas property),
below inversion curve only

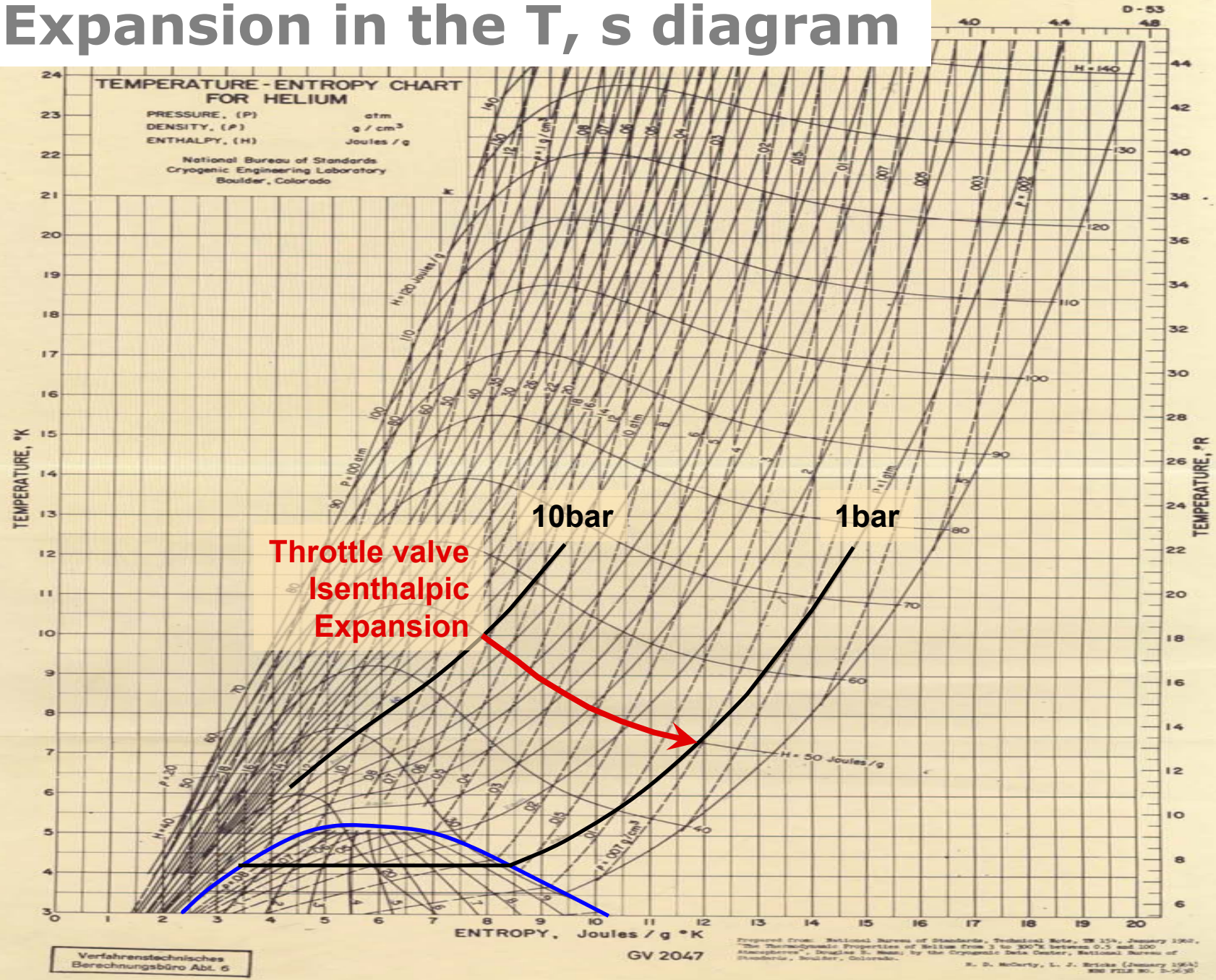


b) Expansion machine
isentropic change of state
work is extracted from the fluid

$$\Delta S_{\text{ideal}} = 0$$

⇔ big effect at any starting temperature
(ideal gas property)

J-T Expansion in the T, s diagram

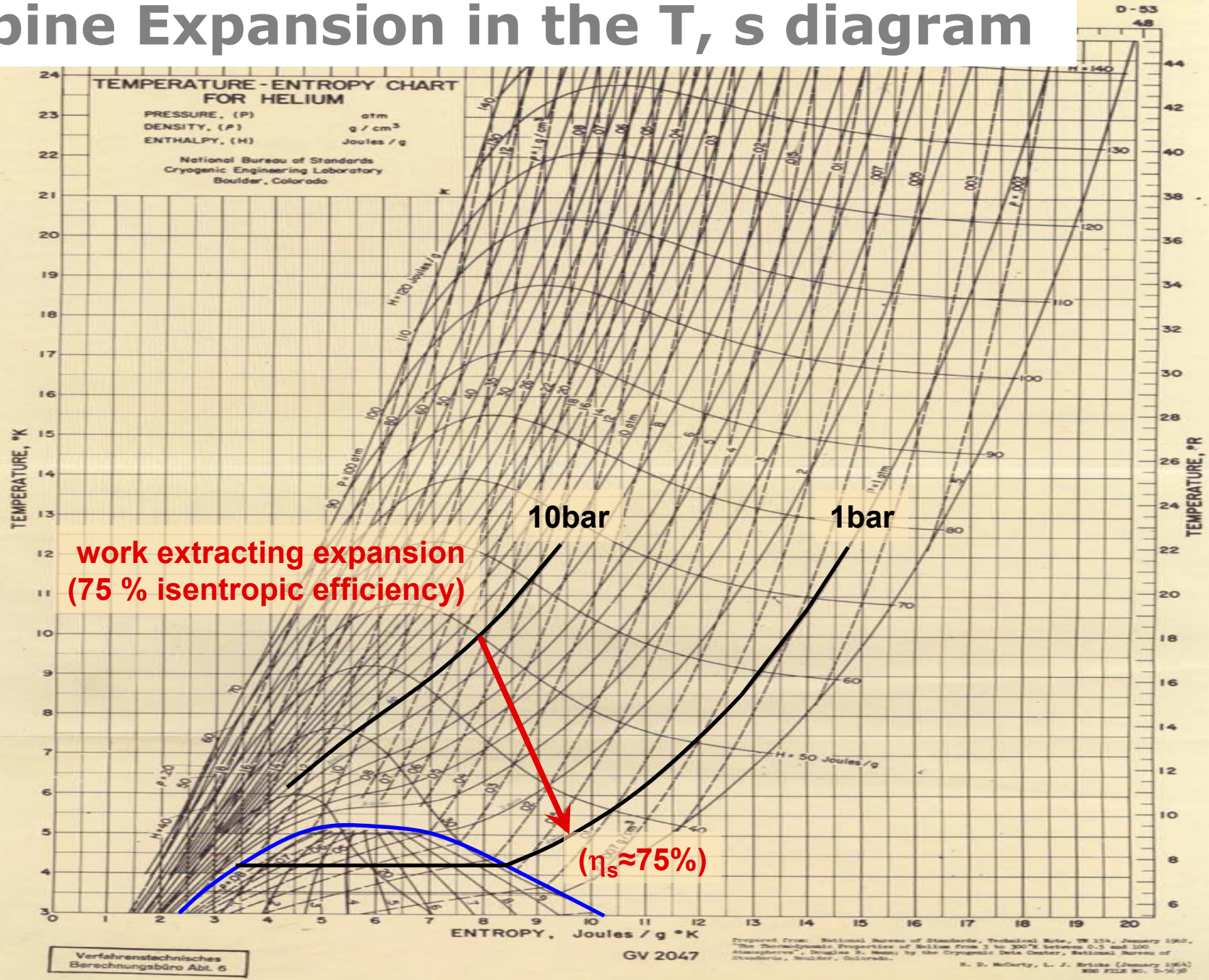


Verfahrenstechnisches
 Berechnungsbüro Abt. 6

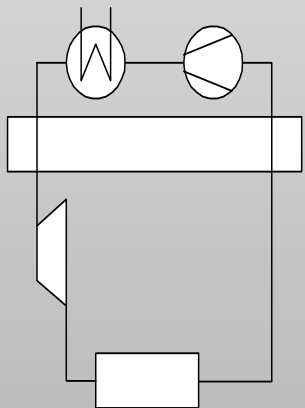
GV 2047

Prepared from: National Bureau of Standards, Technical Note, TN 154, January 1967.
 "The Thermodynamic Properties of Helium from 3 to 300°K between 0.5 and 100
 Atmosphere", Douglas S. Messer, by the Cryogenic Data Center, National Bureau of
 Standards, Boulder, Colorado.
 H. D. McCarty, L. J. Eriks (January 1964)
 NBS FILE NO. 3-5635

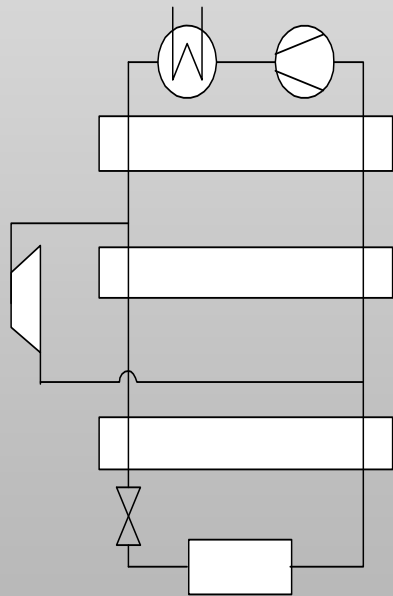
Turbine Expansion in the T, s diagram



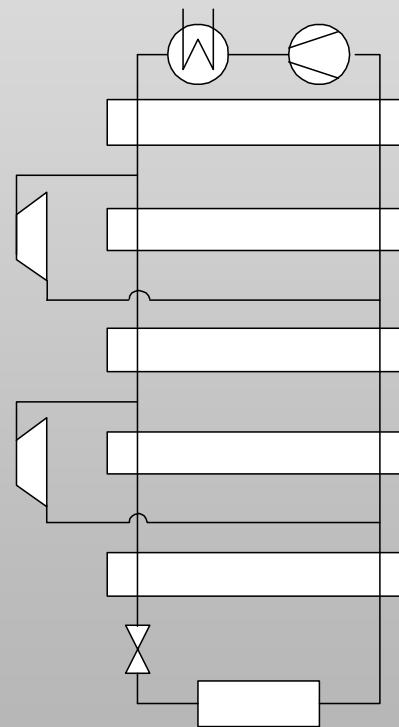
Basic Refrigerator Cycles



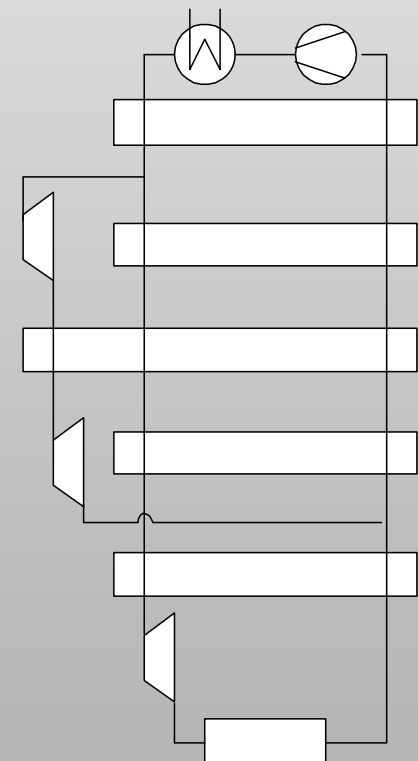
Brayton



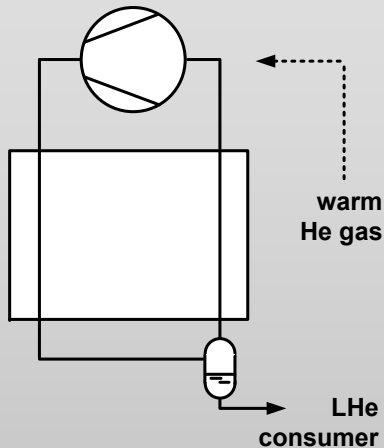
Claude



Expanders in parallel
(Collins)



Expanders in series
plus wet expander



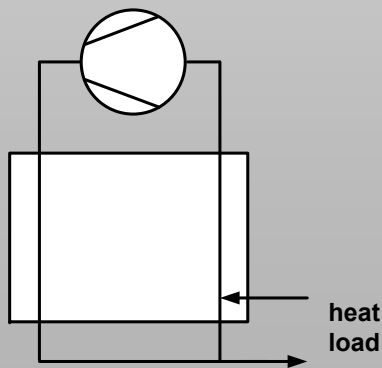
Liquefier

often only evaporation enthalpy used (20.4 kJ/kg)

(cold gas warm-up: 1500 kJ/kg)

standard liquefier: 10 ... 200 l/h

bulk liquefier: ~ 1000 ... 4000 l/h



Refrigerator

heat load (e.g. cavity cryostat)

directly connected via transfer line + cold gas return

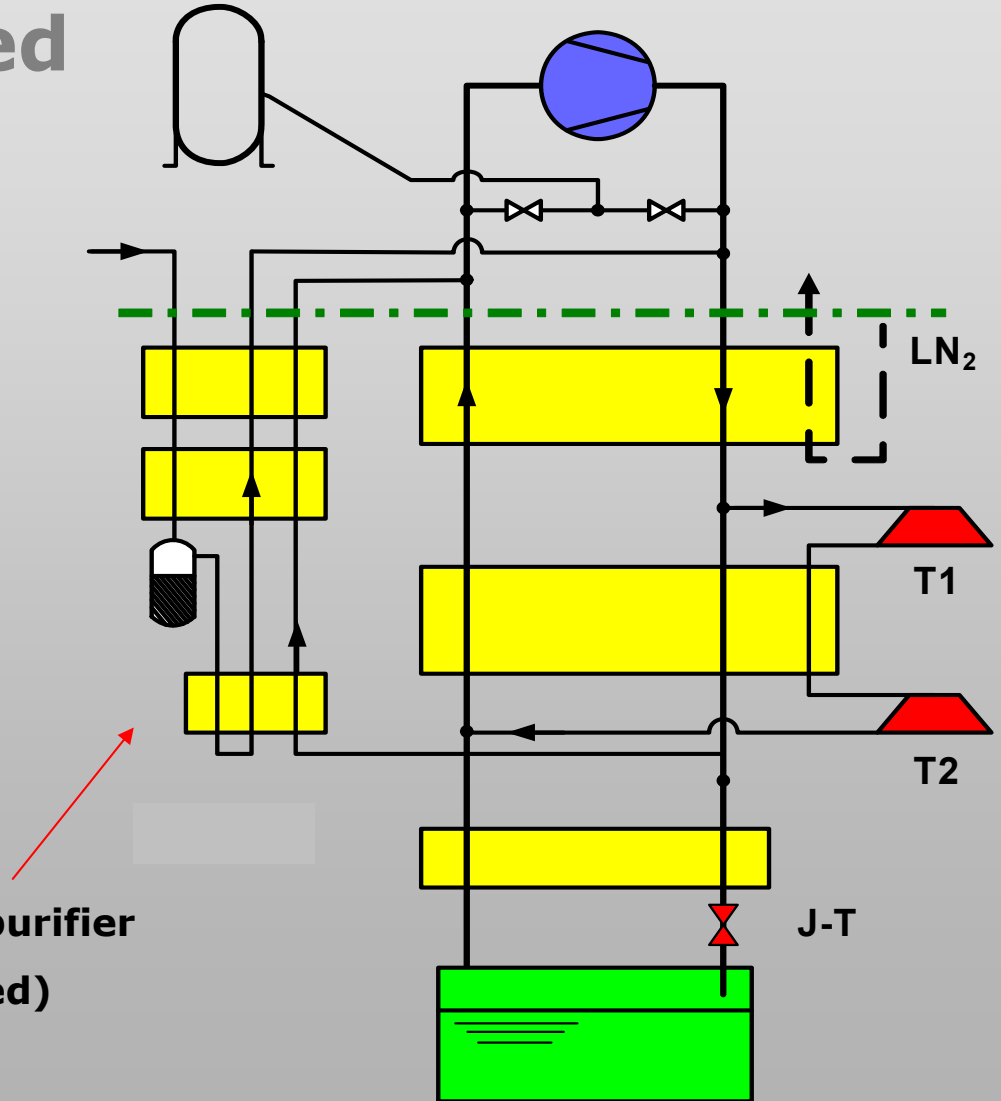
0.1 ... 20 kW @ 1.8 ... 5 K

Components needed

typ. helium liquefier:

- (warm) cycle compressor
- buffer tank
- counter flow heat exchangers
- (optional) LN₂ precooling
- expansion Turbines
- J-T throttle valve
- Cold box

integrated freeze-out purifier
(for impure helium feed)



Helium Expansion Turbines

Motivation:

isentropic Expansion
without cold piston
maschine

Problems:

- small mass flow
- high circumferencial speed
- need for high isentropic efficiency

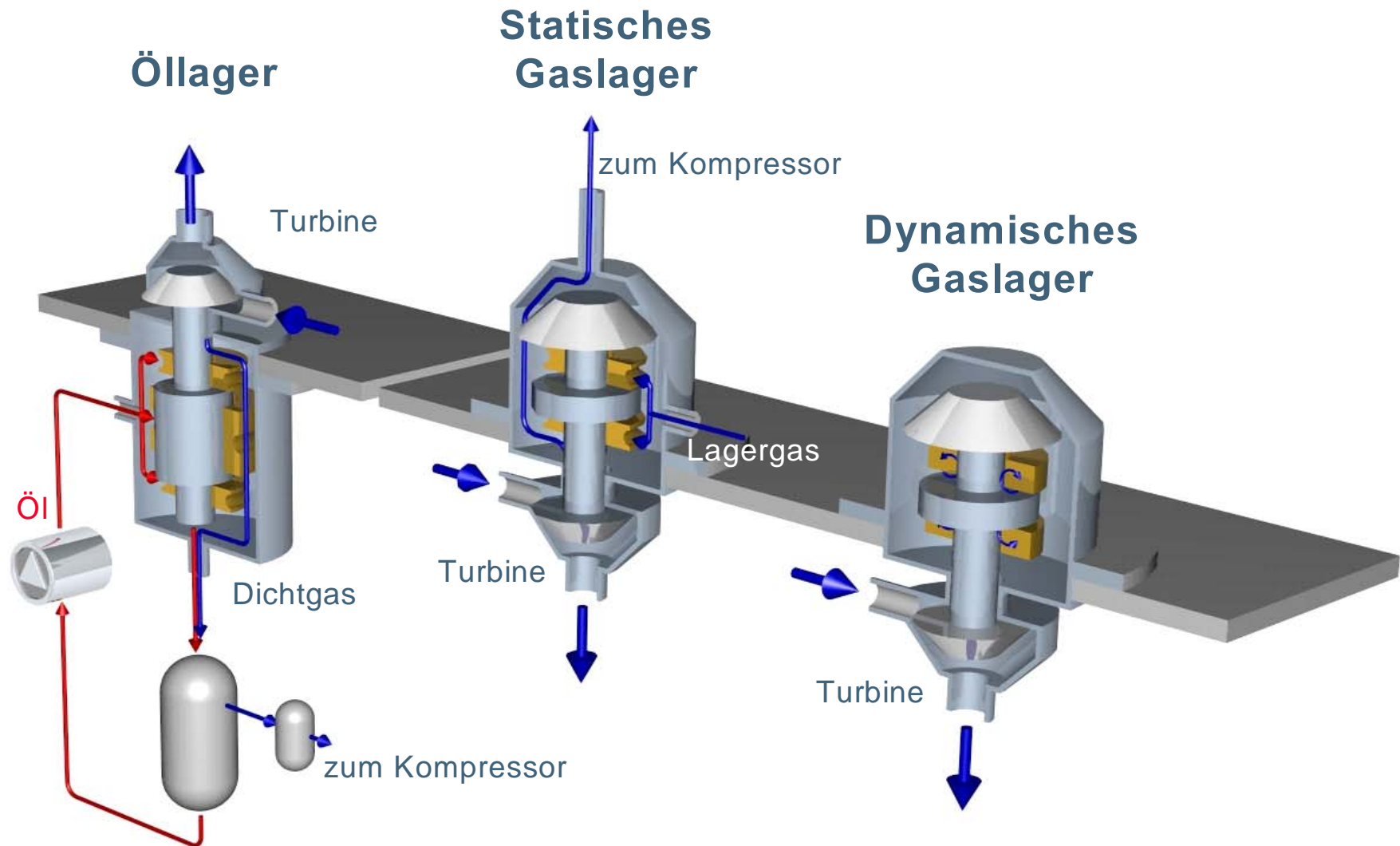


rotational speed

up to 5400 s^{-1}



oil- or gas bearing
exclusively



Helium Expansion Turbines

axial and radial gas bearing; operational speed 4500 s^{-1} typically



recently optimized:

- blades geometry
- clearances
- heat fluxes

isentropic efficiency

90th: $\eta_s \approx 65 \%$

today: $\eta_s \approx 75 \dots 80 \%$

↘ **50 % more
cooling power !**

Cycle Compressors



today: oil-lubricated screw compressors

(followed by oil removal system
down to ppb level !)

one-stage 1,05 bar → ca. 14 bar

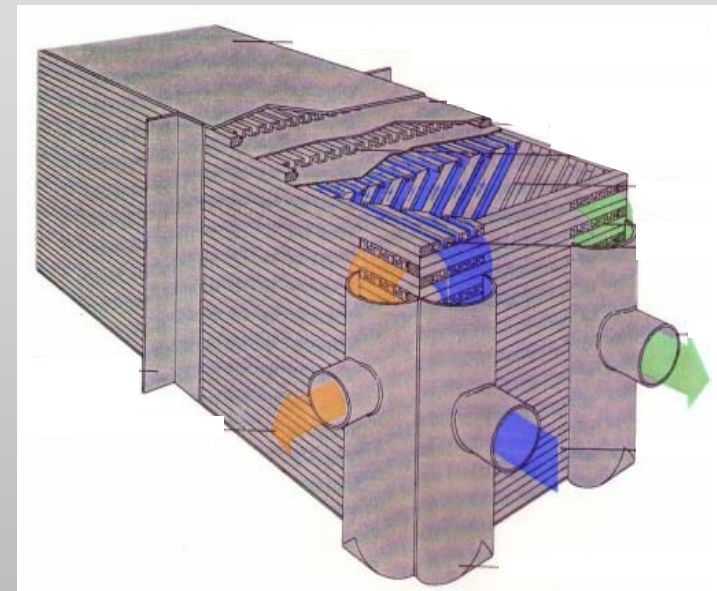


input power 50 kW ... MW

- expensive
- efficiency ~ 50 %

Heat Exchangers

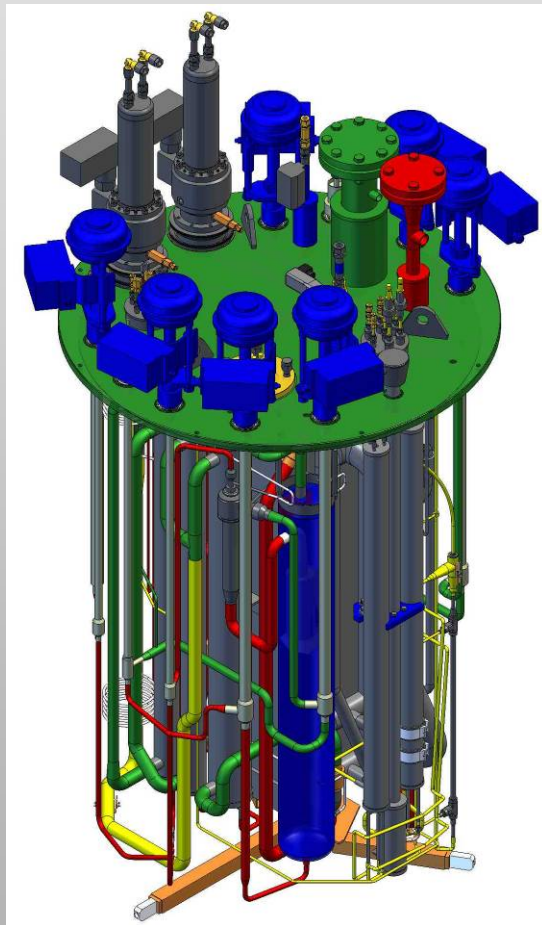
**Aluminium plate-fin
counterflow heat exchangers
vacuum-brazed**



- very reliable
- excellent efficiency ($\Delta T_{\text{in/out}} \approx 3 \text{ K}$)

Coldbox

- vacuum isolated
- vertical arrangement: all components mounted at top flange



Transfer Lines



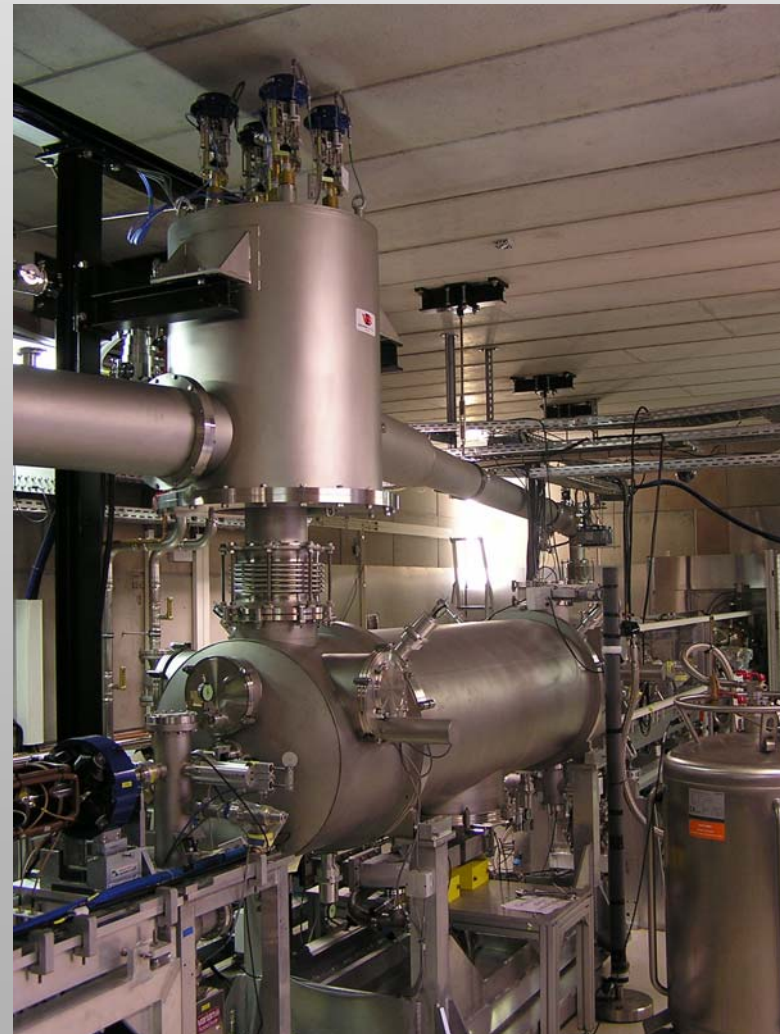
**vacuum isolated
+ thermal shield**

Transfer Lines

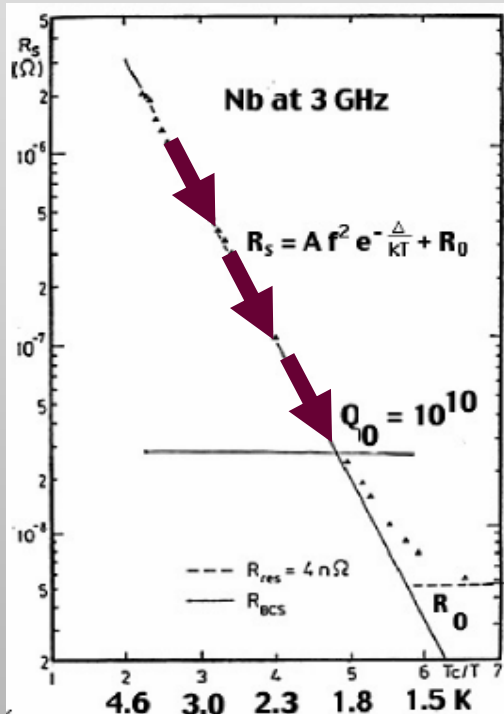


distribution box with heat exchanger

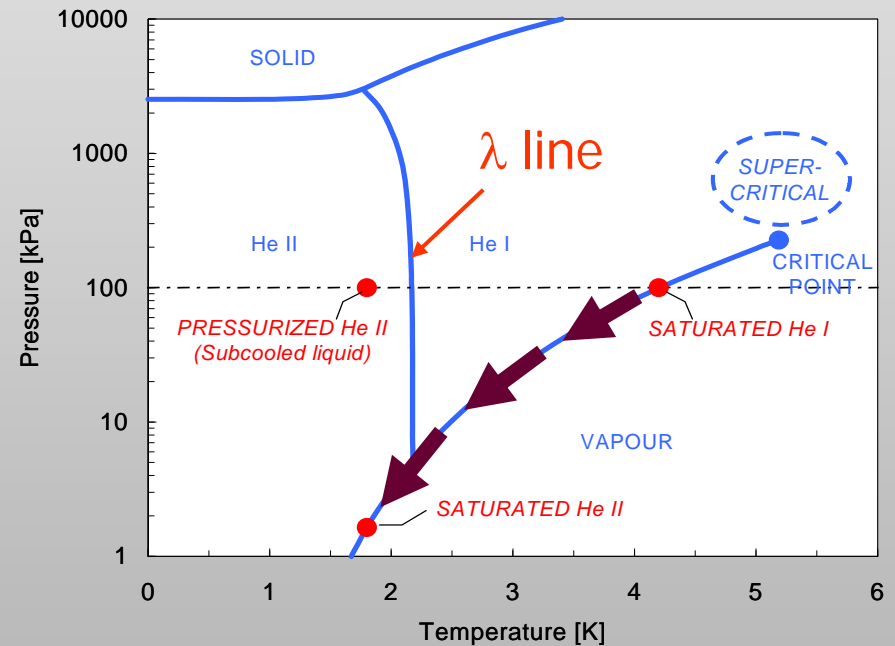
ELBE transfer line + valve box



Quest for lower working temperatures

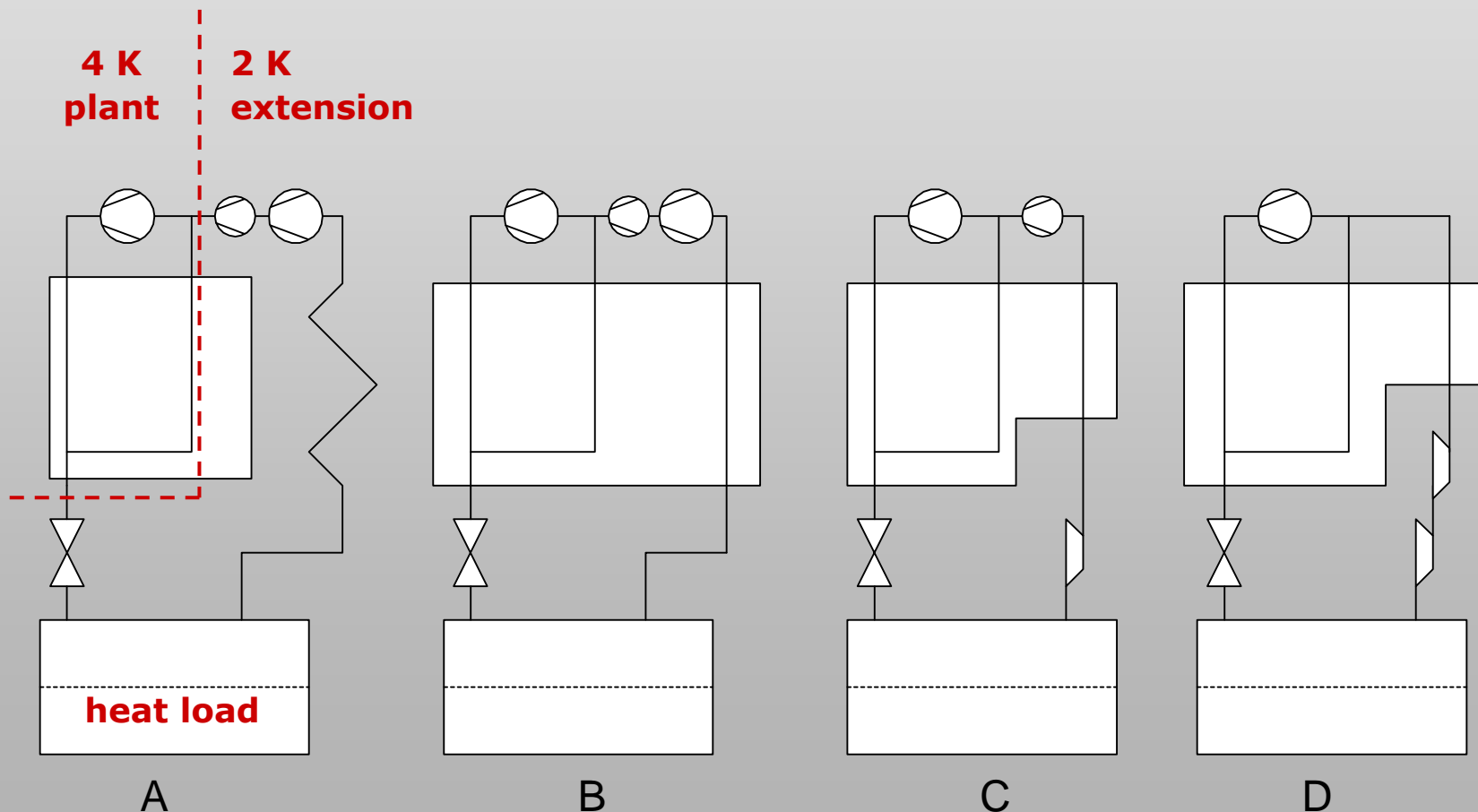


- + much less power dissipation
in rf cavities
- + I_c , B_c gain for sc magnets



- pumped LHe bath
(subatmospheric system)
- increase in power consumption (Carnot)

Subatmospheric (LHe II) helium plants



Subatmospheric (LHe II) helium plants

A: heating of helium return gas to ambient + warm vacuum pumps



DESY VUV-FEL Linac;

DESY TTF supply:

4 rotary vane pumps

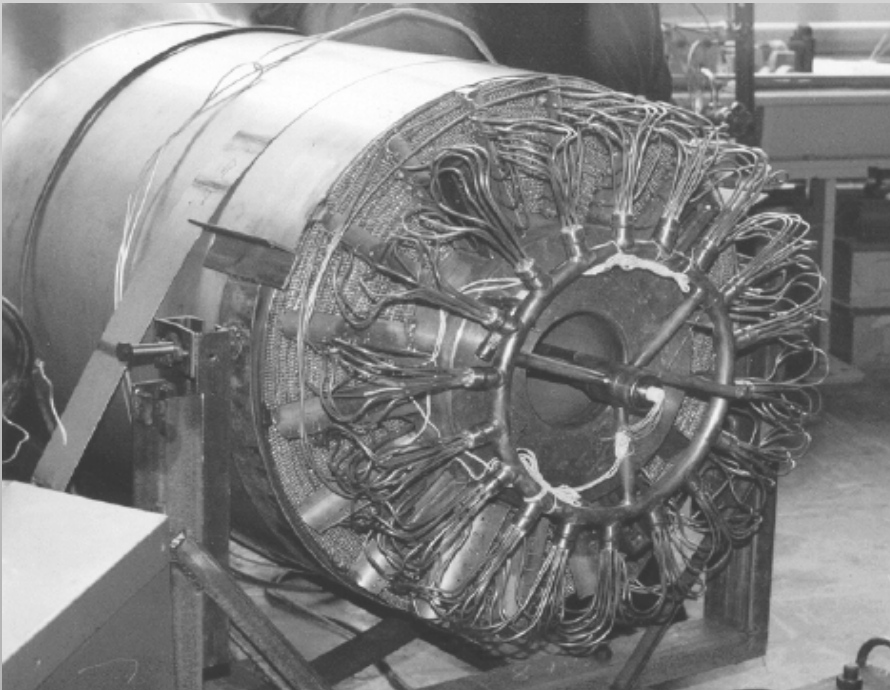
+ 3 stages of roots blowers

10 g/s He;

10 mbar \Rightarrow 1.05 bar

Subatmospheric (LHe II) helium plants

B: demanding, large heat exchanger necessary
(low density helium return gas)



DESY :

3.5 K ⇨ **280 K**
31 mbar **29 mbar**

7.5 K ⇩ **300 K**
12 bar **12 bar**

Subatmospheric (LHe II) helium plants

C: cold compressor(s) necessary

Cold Compressor Cartridges of 2.4 kW @ 1.8 K Refrigeration Units

IHI-Linde



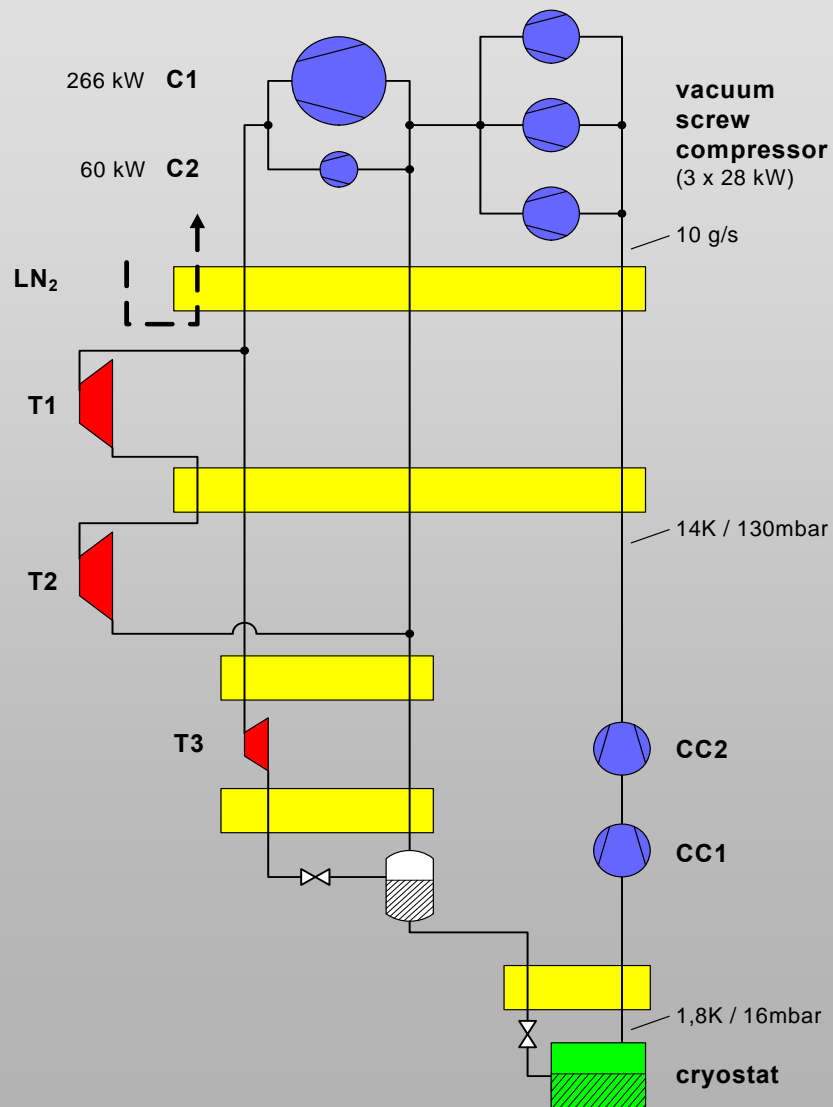
1st stage



Cold compressor impeller



The four-stage LHC cold compressors

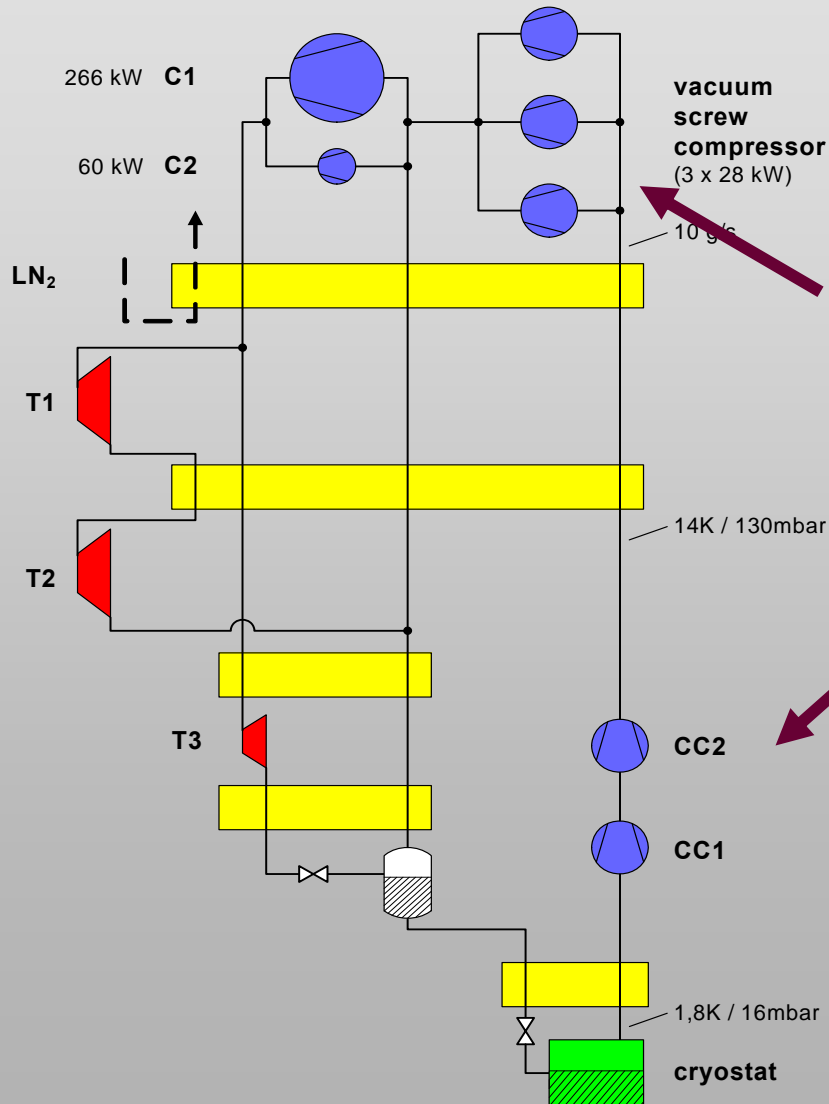


FZ Rossendorf, ELBE accelerator



Helium Refrigerator 220 W @ 1.8 K
(fourth in size all over Germany!)

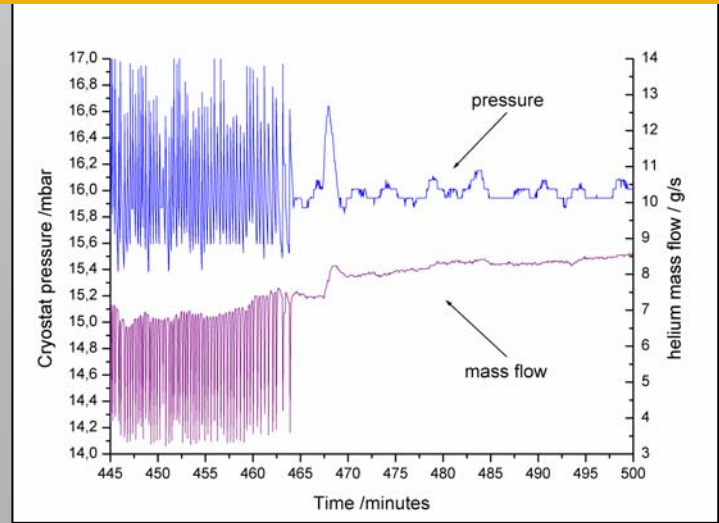
ELBE Helium Plant



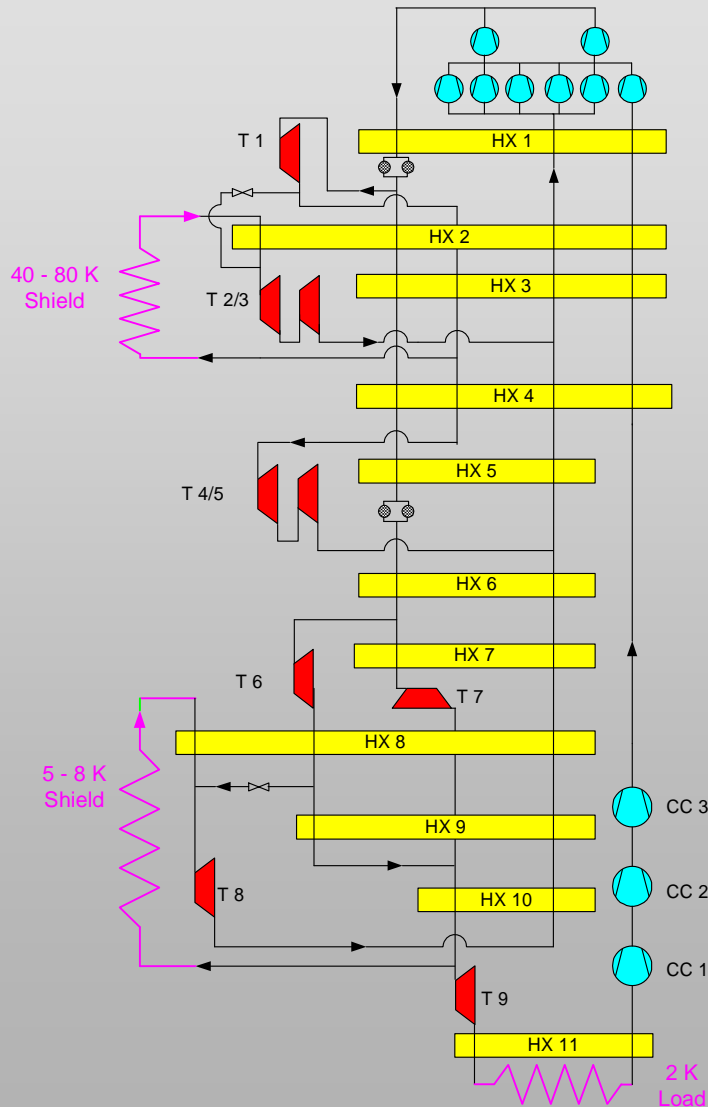
Complications with the subatmospheric part:

**local overheating \Rightarrow oil cracking
 \Rightarrow para-formaldehyd formation + deposition**

„1 Hz“ phenomenon: wrong cold compressor operating map in the beginning \Rightarrow oscillations due to stall regime at part load conditions



“High-end” Helium Plant



Conceptual design for DESY, TESLA:

8 cycle compressors in two stages

9 expansion turbines

3 cold compressors

heat loads at three temperatur levels

Maximum Efficiency

Carnot limit:

$$\text{COP}_{\text{ideal}} = Q/W = T_o / (T_{\text{amb}} - T_o)$$

for full reversible process,
perfect components, ...

$$77 \text{ K: } \text{COP}_{\text{ideal}} \approx 0.25 \quad (3 \text{ W/W})$$

$$4.2 \text{ K: } \text{COP}_{\text{ideal}} \approx 0.014 \quad (70 \text{ W/W})$$

$$1.8 \text{ K: } \text{COP}_{\text{ideal}} \approx 0.006 \quad (166 \text{ W/W})$$

Carnot fraction: $\eta := \text{COP}_{\text{real}} / \text{COP}_{\text{ideal}}$

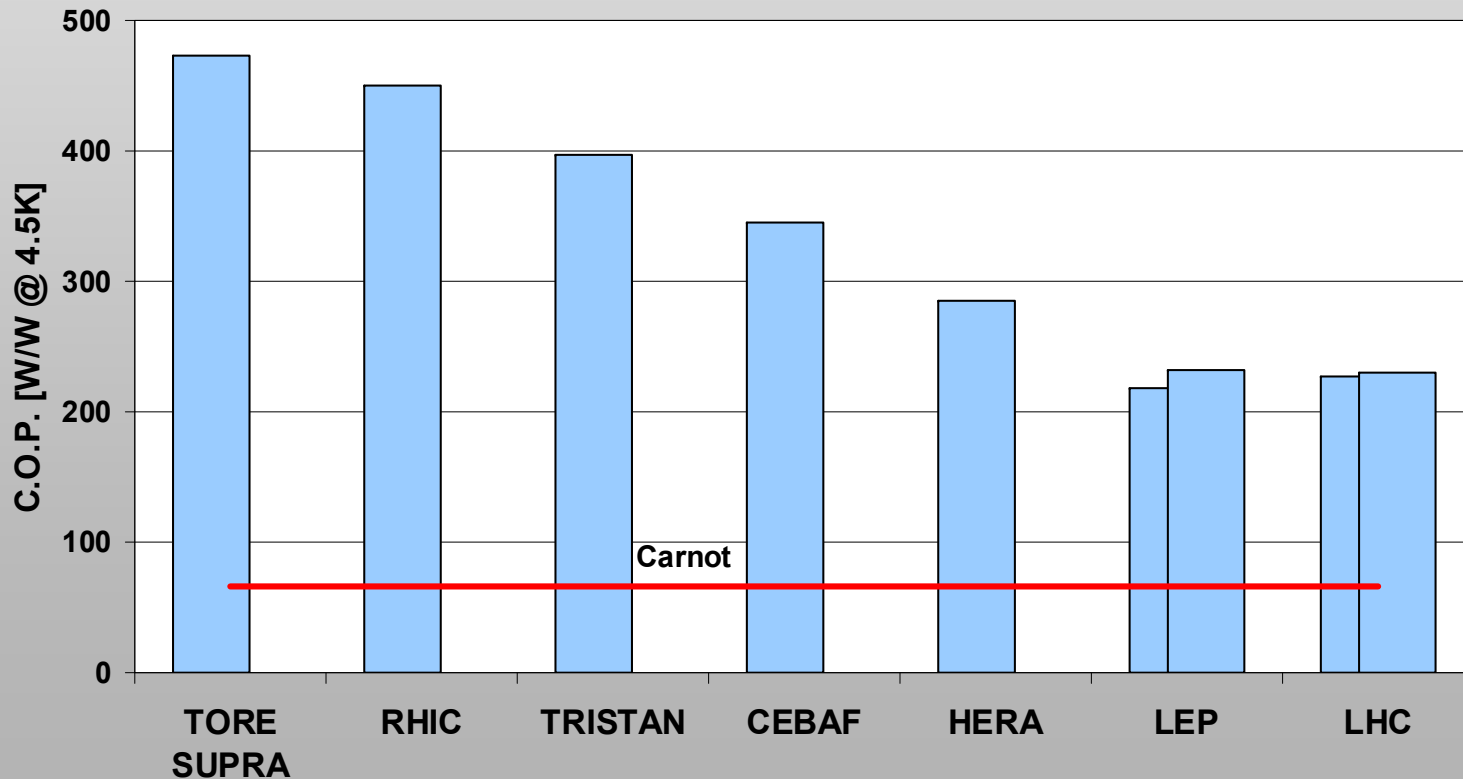
He Plants: $\eta \approx 0.01 \dots 0.35$

e.g.: input power $P_{\text{el}} \approx 0.5 \text{ MW}$

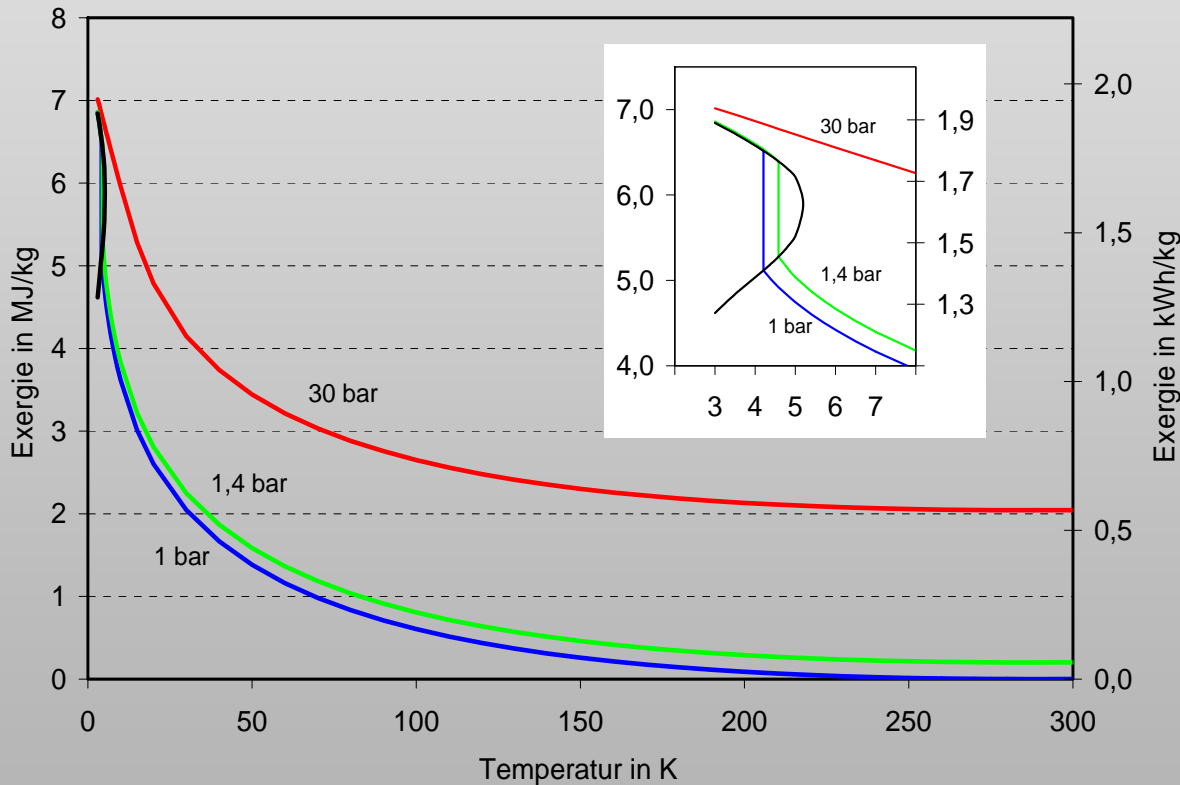


cooling power @ 1.8 K: 200 W

COP of Large Helium Refrigerators

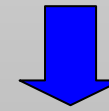


Liquefier Efficiency: Exergy Analysis



Minimum energy input for complete liquefaction from 288 K at 1 bar:

$$6.52 \text{ MJ/kg} = 0.23 \text{ kWh/l}_{\text{LHe}}$$



state-of-the-art:

$$2 \text{ kWh/l}_{\text{LHe}}$$

$$\left. \begin{array}{l} 10^5 \text{ l}_{\text{LHe}}/\text{year} \\ 0,12 \text{ €/kWh} \end{array} \right\} 24\,000 \text{ €/year operational costs}$$

$$E_{\min} = m \cdot [h_o - h_u - T_u \cdot (s_o - s_u)] = m \cdot (e_o - e_u)$$



**Central Helium Liquefier TU Dresden
(standard plant of the 80th):**

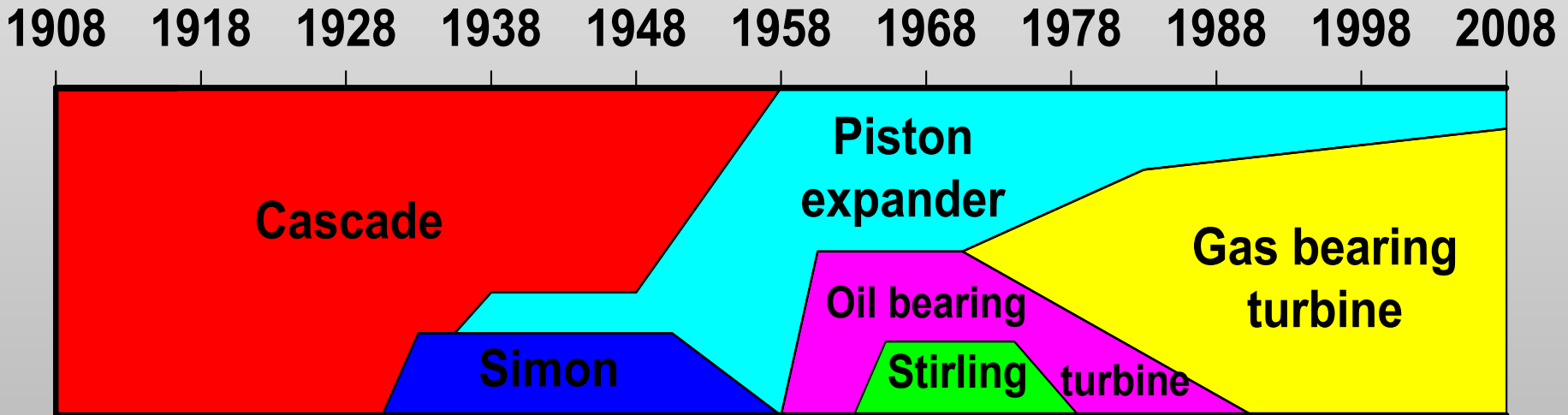
$4.5 \text{ kWh} / \text{l}_{\text{He}} \Rightarrow \eta \approx 0.05$



State-of-the-art helium liquefier
capacity 30 ... 120 l LHe/h

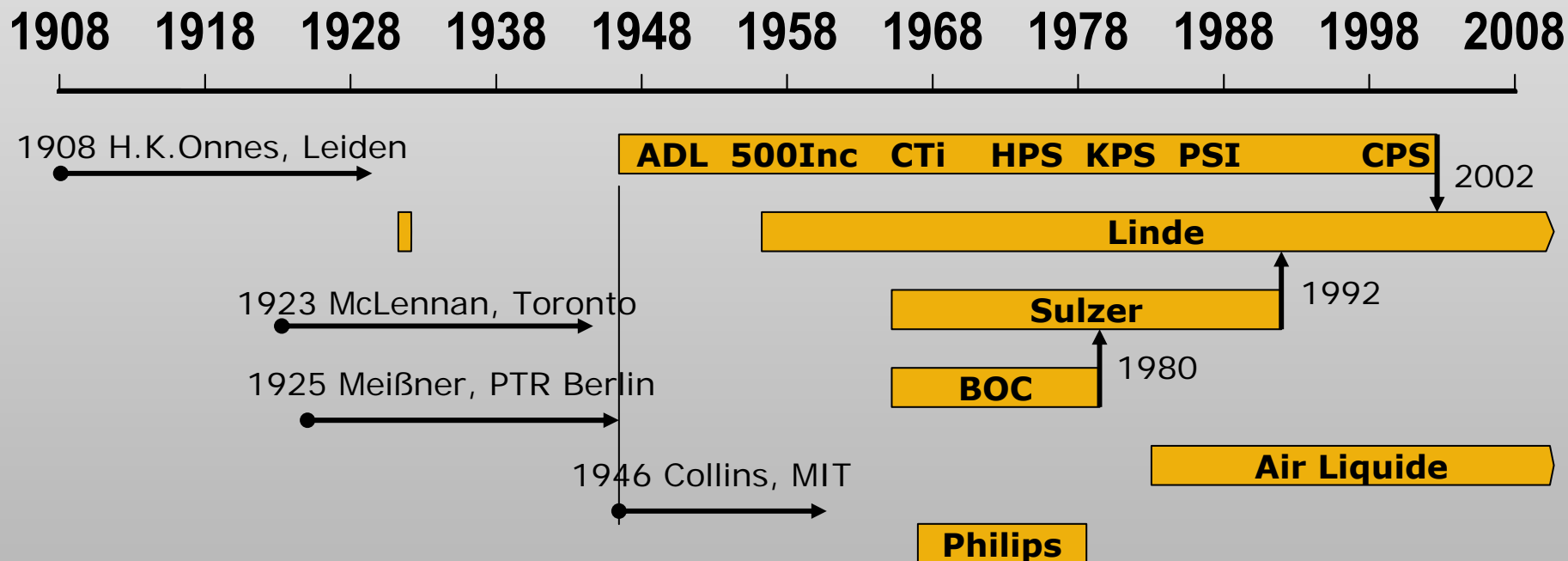
2 kWh / l_{LHe} ⇒ η ≈ 0.012

“Evolution” of Helium Plant Technology



- ⇒ 1. clear trend towards turbine plants with gas bearing
2. concentration on suppliers with own turbine development

“Evolution” of Suppliers

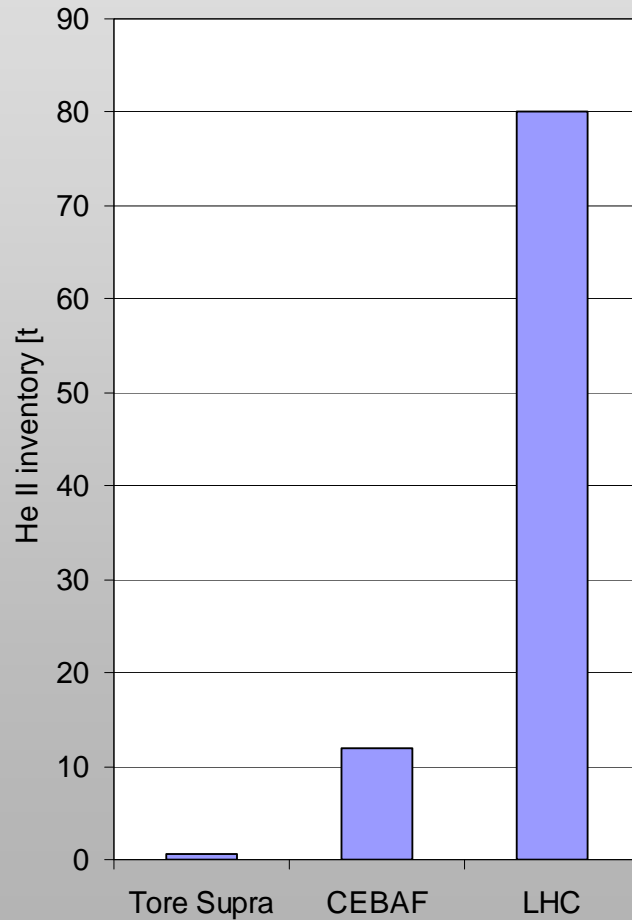


From the very beginning up to the present day:

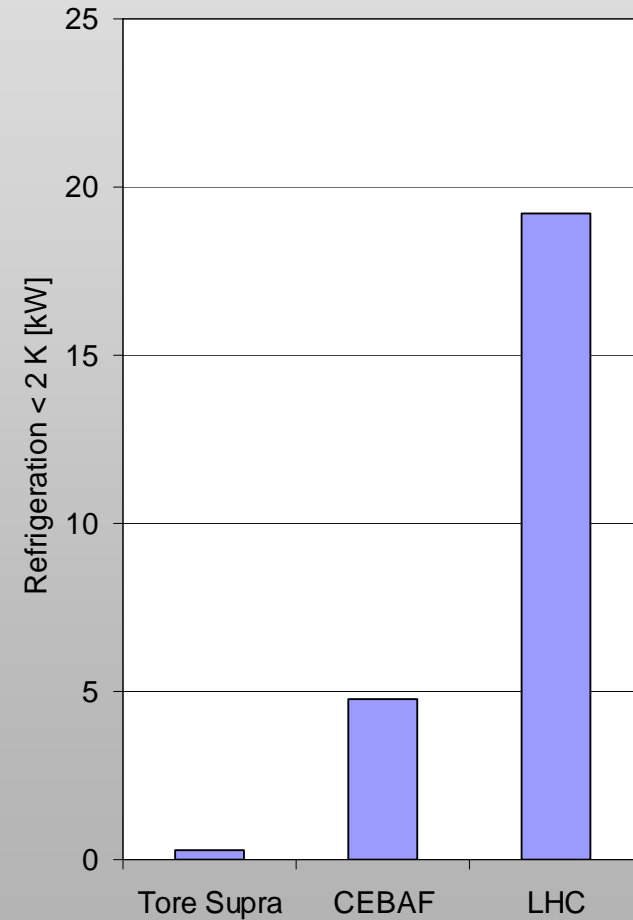
always excellent co-operation between academic research and industry;

Innovations triggered by demanding customers /particle accelerators

He II inventory



Refrigeration power < 2 K



Helium Inventory



250 m³ @ 2 MPa Gaseous Helium Tanks



Helium Sources

**Helium extracted as by-product
from natural gas**

**helium concentration:
traces ... 0.1 % ... 6 %**

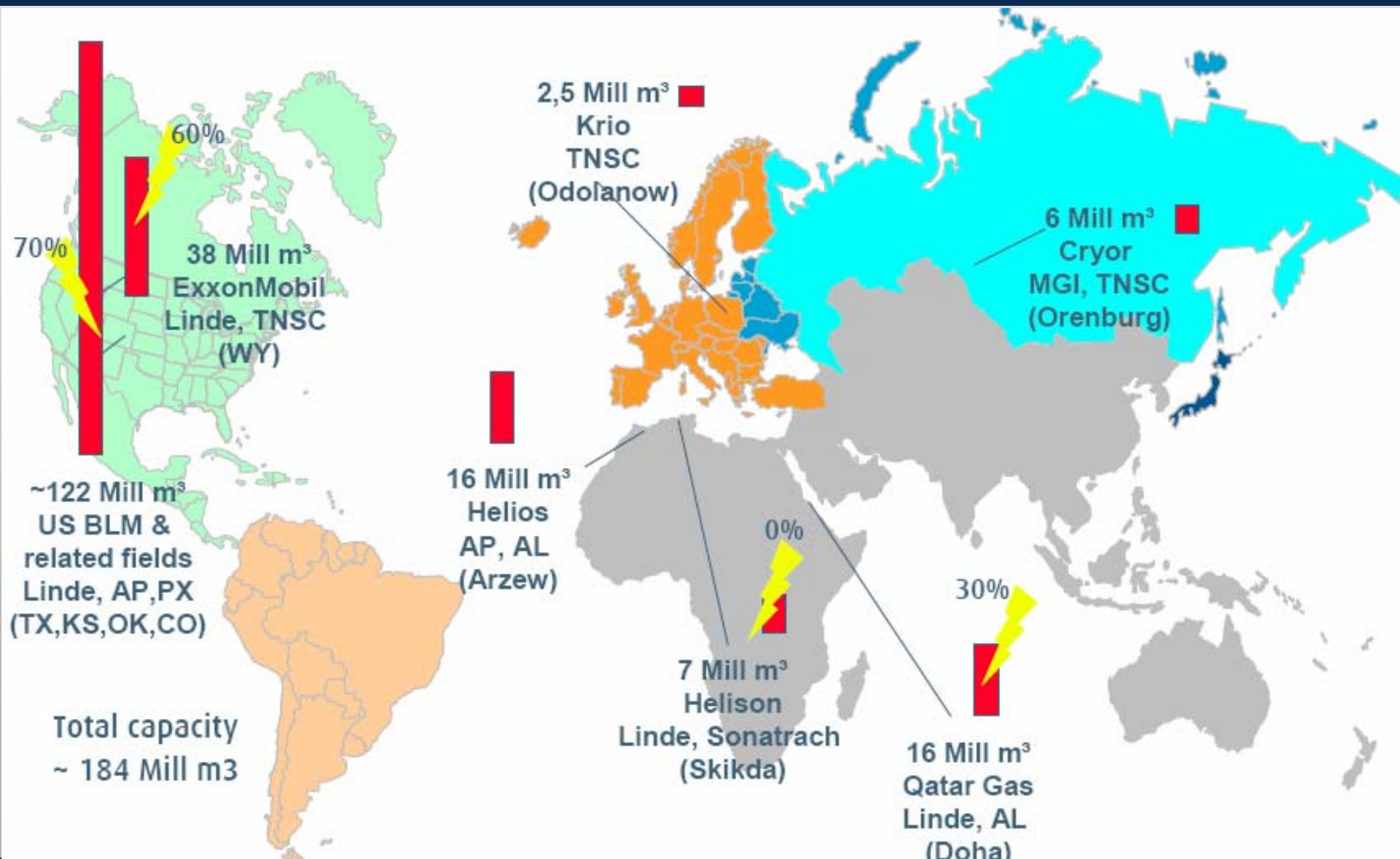
worldwide demand:

**75 tons/day actually
(1/4 of that for cryogenics)**

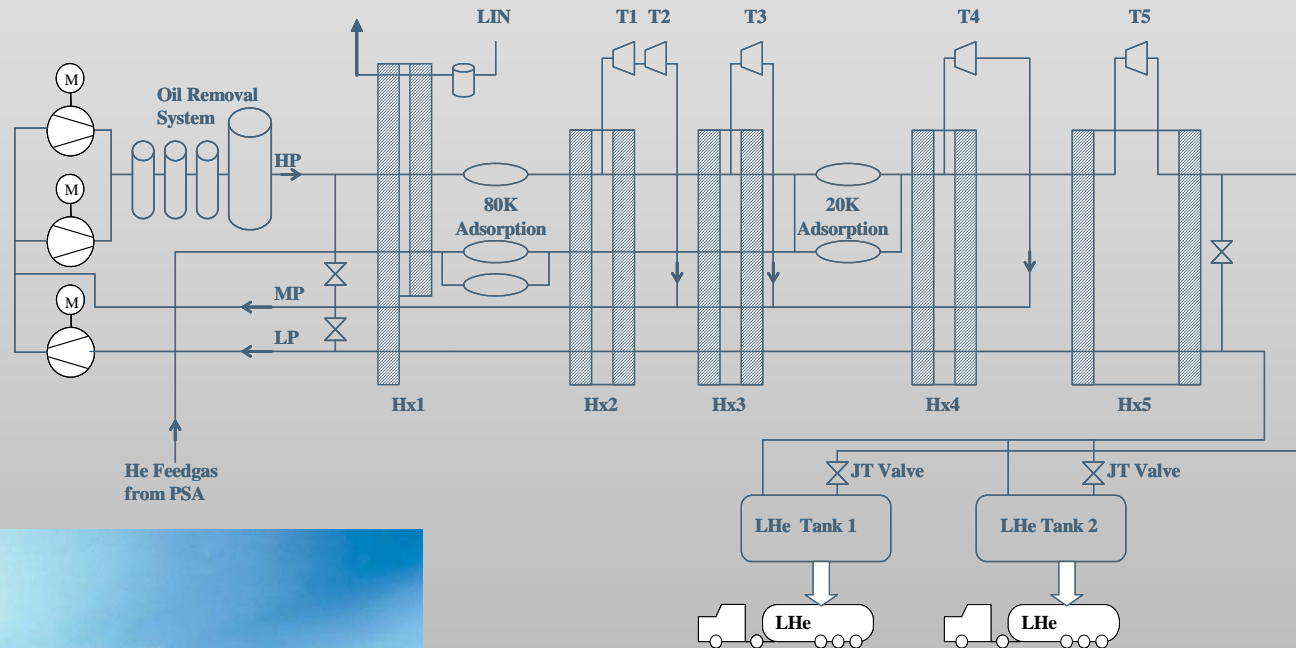
	helium resources (in 10 ⁶ m ³), figures from 2000	helium resources / -sales (in 10 ⁶ m ³), figures from 2007
USA	11 100 ^a	8 200 ^a / 138 ^b
Qatar	(among „others“)	10 000 / 5,5
Algeria	2 100	8 300 / 20
Russia	6 700	6 700 / 6,4
Canada	2 100	2 000 / -
China	1 100	1 100 / -
Poland	280	280 / 3
others	2 800	2 800 / -
total	26 180	39 000 / 173

^a incl. Cliffside storage field (national helium reserve)

^b 80 · 10⁶ m³ production + 58 · 10⁶ m³ withdrawal from Cliffside



Helium Facility Skikda / Algeria



In operation since 2006;
natural gas / He separation and
liquefaction (3000 I_{LHe}/h);

11 000 gal LHe overseas

transport container

Helium Resources

worldwide helium demand permanently rising over the last decades

new extraction facilities built or planned

actually cheap helium sold from the USA (liquidation of the Cliffside National Helium Reserve)

some prominent rich sources are fading out

⇒ **helium price strongly increased**

⇒ **worldwide bottlenecks with helium supply**

sommer 2000

autumn 2001

autumn 2005

autumn 2006

autumn 2007

spring 2008

....



Lesson to learn:

- **Helium is a noble and a rare gas**
- **it will become quite expensive in future**
- **effective use + gas recovery are essential**



Thank you for your attention !

Questions ?